

4.46 $\sin x = x - x^3/3! + x^5/5! - \dots$ and so $\sin(\alpha \pm \beta) = (\alpha \pm \beta)[1 - (\alpha \pm \beta)^2/6]$ using Snell's Law $\theta_t(1 - \theta_t^2/6 + \dots) = (\theta_i/n)(1 - \theta_i^2/6 + \dots)$. Use $1\theta_i = n\theta_t$ and the fact that when x is very small $(1 + x)^{-1} \approx 1 - x$ we have $\theta_t = (\theta_i/n)(1 - \theta_i^2/6)(1 + \theta_i^2/6n^2)$ dropping terms higher than the third power in θ_i we get $\theta_t = (\theta_i/n)[1 - (n^2 - 1)\theta_i^2/6n^2]$ and so

$$\theta_i \pm \theta_t = \theta_i \left[1 \pm \frac{1}{n} \left(1 - \frac{n^2 - 1}{6n^2} \theta_i^2 \right) \right].$$

Using Eq. (4.42) and the power series representation of the sine, where terms higher than the third power in θ_i are dropped,

$$-r_{\perp} = \frac{n - 1 + \frac{\theta_i^2}{6n^2}[n^2 - 1 - (n - 1)^3]}{n + 1 - \frac{\theta_i^2}{6n^2}[n^2 - 1 + (n - 1)^3]} = \left(\frac{n - 1}{n + 1} \right) \left(1 + \frac{\theta_i^2}{n} \right)$$

4.49 Compute $dr_{\perp}/d\theta_i$ at $\theta_i = 90^\circ$; we'll use $d\theta_t/d\theta_i = 0$ and then prove it; taking the derivative of Eq. (4.42) we get

$$\begin{aligned} dr_{\perp}/d\theta_i &= -\cos(\theta_i - \theta_t)/\sin(\theta_i + \theta_t) \\ &\quad + \sin(\theta_i - \theta_t)\cos(\theta_i + \theta_t)/\sin^2(\theta_i + \theta_t) \end{aligned}$$

and for $\theta_i = 90^\circ$ this becomes

$$dr_{\perp}/d\theta_i = -\sin \theta_t/\cos \theta_t - \sin \theta_t \cos \theta_t/\cos^2 \theta_t = 2 \tan \theta_t$$

and using Snell's Law, i.e, $\sin \theta_t = 1/n$ when $\theta_i \approx 90^\circ$, and the fact that

$$\cos \theta_t = \sqrt{1 - \sin^2 \theta_t},$$

$$dr_{\perp}/d\theta_i = 2 \tan \theta_t = 2 \sin \theta_t/\cos \theta_t = 2/n \cos \theta_t = 2/\sqrt{n^2 - 1} :$$

this is the rise over the run at the end of the curve where $\theta_i \approx 90^\circ$. Thus if $\alpha_{\perp}$ is the angle made with the vertical $\tan \alpha_{\perp} = \sqrt{n^2 - 1}/2$.

4.77
$$t_{\parallel} = \frac{2 \sin \theta_2 \cos \theta_1}{\sin(\theta_1 + \theta_2) \cos(\theta_1 - \theta_2)}$$

$$t'_{\parallel} = \frac{2 \sin \theta_1 \cos \theta_2}{\sin(\theta_1 + \theta_2) \cos(\theta_2 - \theta_1)}$$

$$t_{\parallel} t'_{\parallel} = \frac{\sin 2\theta_1 \cos 2\theta_2}{\sin^2(\theta_1 + \theta_2) \cos^2(\theta_1 - \theta_2)} = T_{\parallel}$$

from Eq. (4.100). Similarly $t_{\perp} t'_{\perp} = T_{\perp}$.

$$r_{\parallel}^2 = \left[\frac{\tan(\theta_1 - \theta_2)}{\tan(\theta_1 + \theta_2)} \right]^2 = \left[\frac{-\tan(\theta_2 - \theta_1)}{\tan(\theta_1 + \theta_2)} \right]^2$$

$$r_{\parallel}^2 = \left[\frac{\tan(\theta_2 - \theta_1)}{\tan(\theta_1 + \theta_2)} \right]^2 = r_{\parallel}^2 = R_{\parallel}.$$

$$8.17 \quad I' = \text{flux density through middle polarizer} = I_1 \cos^2 \theta \quad (8.24).$$

$$I' = I_1 \cos^2(45^\circ) = I_1/2$$

$$I_2 = I' \cos^2(45^\circ)$$

$$= (I_1/2)/2 = I_1/4$$

$$8.52 \quad J = \begin{bmatrix} \cos \theta \\ \sin \theta \end{bmatrix} = \begin{bmatrix} \cos 45^\circ \\ \sin 45^\circ \end{bmatrix} = \begin{bmatrix} 1/\sqrt{2} \\ 1/\sqrt{2} \end{bmatrix} = \frac{1}{\sqrt{2}} \begin{bmatrix} 1 \\ 1 \end{bmatrix}$$

$$8.58 \quad \begin{bmatrix} 1 & 0 & 0 & 0 \\ 0 & 0 & 0 & -1 \\ 0 & 0 & 1 & 0 \\ 0 & 1 & 0 & 0 \end{bmatrix} \begin{bmatrix} 1 \\ 0 \\ 1 \\ 0 \end{bmatrix} = \begin{bmatrix} 1 \\ 0 \\ 1 \\ 0 \end{bmatrix}$$

Therefore light polarized at 45° is unchanged, as expected.

$$\begin{bmatrix} 1 & 0 & 0 & 0 \\ 0 & 0 & 0 & -1 \\ 0 & 0 & 1 & 0 \\ 0 & 1 & 0 & 0 \end{bmatrix} \begin{bmatrix} 1 \\ 1 \\ 0 \\ 0 \end{bmatrix} = \begin{bmatrix} 1 \\ 0 \\ 0 \\ 1 \end{bmatrix}$$

A horizontal $\mathcal{P}$ -state is changed to an $\mathcal{R}$ state.